



# Fully 3D model of TF coil structures in the 4C code

#### R. Bonifetto, L. Savoldi, R. Zanino

NEMO Group, Dipartimento Energia, Politecnico di Torino, Torino, Italy



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### Outline

- Introduction and background: the 4C code
- Motivation and aim of the work
- Test cases definition
- Results and discussion
- Conclusions and perspective



## **Background: the 4C code**



#### Circuit module [Modelica]

0D pumps, thermal buffers, manifolds, valves, 1D pipes

#### Winding module [FORTRAN]

1D conductors (two-fluid + solids), thermally coupled in transverse 2D





## Focus: the 2D(+1D) structures model

### • ASSUMPTIONS:

- All the He flow paths are in the poloidal direction
- Forced flow cooling
- Major polidally non-uniform driver located in the WP
- <u>Peclet number</u> (in the *poloidal* direction):  $\frac{conduction time}{advection time} \sim 100-1000 \rightarrow \text{neglect poloidal} + \text{heat conduction}$ 
  - → most of the heat is advected by SHe between poloidal cuts (<u>1D</u> <u>poloidal heat transfer</u>)
  - ➔ the most important T gradient in structures is *across* SHe flow direction (<u>2D radial-toroidal</u> <u>conduction</u>)



**EU DEMO TF (3D) coil** 





## The 4C model of the EU DEMO TF coils

- WP with inter-turn and inter-layer thermal coupling
- Steel casing (thermally coupled with WP)
- Casing cooling channels (CCCs)
- External cryogenic circuits





## 4C Verification&Validation including structures

[RZ.and L. Savoldi., Multi-scale approach and role of validation in the thermal-hydraulic modelling of the ITER superconducting magnets, IEEE TAS 2013]









# Motivation

- The 4C code is now used in the <u>design</u> phase of forthcoming tokamaks (EU DEMO, DTT, ...)
- → new needs:
- Investigate transients driven by a strongly *non-uniform* power deposition <u>in the casing</u> (e.g. localized conductive heat load)
- Analyze <u>new designs</u> with non-(only-)poloidal cooling paths
- Simulate operation/accident at <u>reduced/no He flow</u> (LOFA, baking, ...)
- Investigate <u>complex 3D features</u> of the structures







## Aim of the work

- Develop and test a first (simplified) 3D model of the coil structures
  - Demonstrate the full 3D model feasibility with the same tool (FreeFEM++) already used to model the 2D heat conduction in the structures cuts
    - $\rightarrow$  straightforward integration in the 4C architecture
  - Assess the difference/improvement in the simulation results





## **Test geometry**







# **Simulation setup**







### **Test case 1: "thin" structures**



Poloidally distributed heating (nuclear, eddy, radiative, ...)

> Conduction time among cuts (*along* SHe flow direction) is long (~1000 s)

Conduction in the structures *across* SHe flow direction is predominant! (conduction time ~10 s)





### **Test case 2: "thick" structures**



Poloidally localized heating from GS, PF coil supports, ...

Conduction time still long (~1000 s) both *across* and *along* SHe flow direction  $\rightarrow$  heat will flow also *along* SHe flow direction

Conduction in the structures *along* SHe flow direction no more negligible!













a good approximation of the structures behavior SHe flow at 4.5 K, 6 bar



# **Results: CICC (I)**



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### For **"thick" structures**:

- The peak jacket T can be overestimated by ~0.4 K
- The cable temperature can be locally underestimated by ~0.1 K

The "thinner" the structures, the more similar the CICC temperature profiles for both 2D+(1D) and 3D structure models

Effect of heat conduction in the jacket







## **Results: CICC (II)**



Only the jacket T is (locally) affected by the increase of the cut number

- No effect on the cable T distribution
- Conduction along the SHe flow direction neglected → the pre-heating effect of the conduction in the structures is not captured even for increasing cut numbers



## **Reduced Peclet number case**

 Mimic a partial LOFA (~no flow in WP): advection time increases
→ Peclet ~1-10

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T [K]

12.601 12.188

11.776 11.363

10.95

10.538 10.125

9.7123 9.2996 8.887 8.4743 8.0616 7.6489 7.2363 6.8236 6.4109 5.9983 5.5856 5.1729 4.7602

• "Thick" structures case

Fully 3D

problem

conduction





2D(+1D)

**3D** 



## **Drawback and workaround**

 Full 3D model of the structures → increased computational cost (~10 times longer!)



 full 3D model only in the coil sections where it is necessary (e.g. gravity support region, ...)

 set of 2D cuts in the other regions (2D+1D model)





## **Conclusions and perspective**

- The new, design-oriented applications of the 4C code ask for a more detailed modeling of the TF structures
- The possibility to build the full 3D model of the structures within the 4C code has been demonstrated
- The full 3D model has been benchmarked against the validated 2D(+1D) model highlighting:
  - Limited (but not negligible) impact on the cable temperature
  - Relevant impact on the structures temperature

#### In perspective:

- The (full or partial) 3D model can be adopted to describe complex geometries / cooling solutions or to investigate transients involving reduced-cooling conditions
- The full 3D model can be extended to
  - Include other piece of physics (e.g. thermo-mechanics)
  - Develop electromagnetic models to compute eddy currents in the casing





## Thank you for your attention!